TP 14220E

Effect of Surface Conditions on the Friction Coefficients Measured on Winter Surfaces

Prepared for Transportation Development Centre On behalf of Aerodrome Safety Branch of Civil Aviation Transport Canada March 2003

by

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by

G. Comfort BMT Fleet Technology Limited

March 2003

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Since some of the accepted measures in the industry are imperial, metric measures are not always used in this report.

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	 Analyses portant sur chaque surface – là où c'était possible, les coefficients de frottement obtenus à l'aide des appareils de mesure ont été comparés aux mesures du Coefficient canadien de frottement sur piste 							
	(CRFI, pour Canadian Runway pour Aeronautical Information P	<i>Friction Index</i>) donne <i>ublication</i>).	es dans la Pub	lication d'inform	ation aerona	autique (AIP,		
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Brahim Djimet carried out the database searches used for these analyses.

EXECUTIVE SUMMARY

Testing has been under way at North Bay and elsewhere since 1996 as part of the Joint Winter Runway Friction Measurement Program (JWRFMP). The main research objectives are to:

- Compare friction readings from various devices
- Evaluate the relationship between ground vehicle and aircraft friction coefficients

The results of this testing have led to the generation of a large information database regarding friction coefficients on winter surfaces.

The general objective of this project was to investigate the effect of surface conditions on friction coefficients. The work comprised two general parts: analyses for individual surfaces and correlation analyses.

Analyses for Individual Surfaces

This work investigated the friction coefficients measured for various surface types such as ice, snow, packed snow, and dry and wet pavement. Three devices were analyzed:

- 1. Electronic Recording Decelerometer (ERD)
- 2. Transport Canada's Surface Friction Tester (TC SFT'79)
- 3. Instrument de Mesure Automatique de la Glissance (IMAG)

The following issues were examined:

- Range and distribution of friction coefficient values by surface and friction-measuring device
- Effect of surface temperature
- Effect of snow depth for surfaces with loose snow

The results were compared to the Canadian Runway Friction Index (CRFI) guidelines given in the Aeronautical Information Publication (AIP). The results varied from device to device and from surface to surface, which makes it difficult to infer general conclusions. It was, however, commonly observed that the ranges of values observed in the JWRFMP were larger than those given in the AIP.

Correlation Analyses

This work evaluated the effects of surface conditions on correlations between measurements recorded by the above devices.

Again, the results varied from device to device and from surface to surface, which makes it difficult to infer general conclusions. However, it was noted that:

- ERD readings on contaminated surfaces were generally higher and more scattered on contaminated surfaces than those for the TC SFT'79 and the IMAG. This probably reflects the fact that the ERD is a locked-wheel test.
- TC SFT'79 and the IMAG showed good correlation for all surfaces.

Recommendations

This was an exploratory project to investigate general trends and relationships. The results obtained here should be followed up with more detailed quantitative analyses to investigate issues such as:

- Variability among the results for different surfaces.
- Degree of confidence that one could have in friction coefficients inferred solely from surface descriptions, in comparison to data obtained with friction-measuring devices.

SOMMAIRE

Introduction

Depuis 1996, des essais ont lieu dans le cadre du Programme conjoint de recherche sur la glissance des chaussées aéronautiques l'hiver (PCRGCAH). Ces essais, qui ont lieu à North Bay et ailleurs dans le monde, ont comme grands objectifs:

- de comparer les valeurs de frottement obtenues à l'aide de divers appareils de mesure
- d'évaluer la relation entre les coefficients de frottement établis à l'aide de véhicules au sol et d'aéronefs

Ces essais ont permis d'accumuler une imposante base de données concernant les coefficients de frottement sur des surfaces contaminées par des précipitations hivernales.

L'objectif principal de ce projet était d'étudier l'effet de l'état de la surface sur les coefficients de frottement mesurés sur celle-ci. Les travaux comportaient deux volets: des analyses portant sur chaque surface et des analyses de corrélation entre les appareils de mesure.

Analyses portant sur chaque surface

Ce travail a consisté à analyser les coefficients de frottement mesurés sur divers états de piste: piste couverte de glace, de neige et de neige compactée, piste sèche et piste mouillée. Trois appareils ont été utilisés:

- 1. le décéléromètre électronique (ERD, pour *Electronic Recording Decelerometer*)
- 2. le glissancemètre de Transports Canada (TC SFT'79)
- 3. l'Instrument de mesure automatique de la glissance (IMAG)

Les questions suivantes ont été examinées:

- Étendue et distribution des valeurs du coefficient de frottement selon la surface et l'appareil de mesure
- Effet de la température de la surface
- Effet de l'épaisseur de la neige, dans le cas de surfaces couvertes de neige folle

Les résultats ont été mis en relation avec les mesures du Coefficient canadien de frottement sur piste (CRFI, pour *Canadian Runway Friction Index*) contenues dans la Publication d'information aéronautique (AIP, pour *Aeronautical Information Publication*). Comme les résultats variaient d'un appareil à l'autre et d'une surface à l'autre, il n'a pas été possible de tirer de conclusion générale. On a toutefois couramment observé que la gamme des valeurs issues du PCRGCAH était plus étendue que celle des valeurs données par l'AIP.

Analyses de corrélation

Cette partie du travail a consisté à évaluer les effets de l'état de la surface sur la corrélation entre les mesures enregistrées par les divers appareils susmentionnés.

Encore une fois, les résultats variaient d'un appareil à l'autre et d'une surface à l'autre, ce qui n'a pas permis de tirer de conclusion générale. Il a toutefois été possible de noter ce qui suit:

- Sur les surfaces contaminées, les lectures faites par l'ERD étaient généralement supérieures à celles obtenues à l'aide du glissancemètre de TC et de l'IMAG, et elles étaient aussi plus dispersées. Cela est probablement attribuable au fait que l'ERD est un appareil qui prend ses mesures avec la roue bloquée.
- Le glissancemètre de TC et l'IMAG ont affiché une bonne corrélation pour toutes les surfaces.

Recommandations

Ce projet à caractère exploratoire visait à cerner des tendances et des liens généraux. Les résultats obtenus ici devraient faire l'objet d'analyses quantitatives plus détaillées afin de clarifier des questions comme:

- la variabilité entre les résultats obtenus pour différents états de piste.
- le niveau de confiance que l'on peut avoir dans les coefficients de frottement déduits uniquement des caractéristiques de la piste, par opposition à des coefficients de frottement mesurés par des appareils.

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GLOSSARY OF TERMS

- AIP Aeronautical Information Publication
- CRFI Canadian Runway Friction Index
- ERD Electronic Recording Decelerometer
- IMAG Instrument de Mesure Automatique de la Glissance (French acronym for friction-measuring device manufactured by the French Civil Aviation Authority)
- IRV IRFI Reference Vehicle
- IRFI International Runway Friction Index
- JWRFMP Joint Winter Runway Friction Measurement Program
- TC SFT'79 Surface Friction Tester device owned by Transport Canada

1. INTRODUCTION

1.1 Background

Testing has been under way at North Bay and elsewhere since 1996 as part of the Joint Winter Runway Friction Measurement Program (JWRFMP). The main research objectives are as follows:

- to compare friction readings from various devices
- to evaluate the relationship between ground vehicle and aircraft friction coefficients

The results of this testing have led to the generation of a large information database [1] regarding friction coefficients on winter surfaces.

1.2 Objective

The general objective of this project was to investigate the effect of surface conditions on friction coefficients. The work comprised two general parts:

- [1] Analyses for Individual Surfaces This work investigated the friction coefficients measured for various surface types such as ice, compacted snow, and others. The results were also compared to the Canadian Runway Friction Index (CRFI) guidelines given in the Aeronautical Information Publication (AIP) [2]. The work investigated the following issues:
 - (a) Range and distribution of values by surface and friction-measuring device the surfaces evaluated included those given in the AIP [2]. Three devices were analyzed:
 - i. Electronic Recording Decelerometer (ERD)
 - ii. Transport Canada's Surface Friction Tester (TC SFT'79)
 - iii. Instrument de Mesure Automatique de la Glissance (IMAG)
 - (b) Effect of surface temperature
 - (c) Effect of snow depth for surfaces with loose snow
- [2] Correlation Analyses This work evaluated the effects of surface conditions on correlations between measurements recorded by the above devices.

2. METHOD AND DATABASE SEARCH PARAMETERS

2.1 Overall Summary

Database search parameters were specified as follows:

- Year and site All years and sites were included in all searches to maximize the size of the data set.
- Speed All speeds were included in all searches. This was done as previous analyses (e.g., [3]) have shown that friction coefficients on winter surfaces are not greatly dependent on speed. The data set was maximized by including all speeds.
- Surface and base conditions Several cases were investigated as described in section 2.2.
- Devices The analyses were limited to the friction coefficients measured by the ERD, the TC SFT'79 and the IMAG (section 2.3). The IMAG was investigated rather than the IRFI Reference Vehicle (IRV) as the IMAG was tested over a longer time span during the JWRFMP.
- Maintenance action In most cases, the searches were made for surfaces that had not been treated with any maintenance action. However, a few searches were made for sanded ice (see section 2.2).
- Time interval between individual friction readings All readings were included. The results were not partitioned by time interval.
- Track section on which the average friction coefficient is computed The analyses were done using average friction coefficients for the whole track section, as opposed to 100 m sections (which is the other option in the search wizard). This selection was made because it maximized the size of the data set, as only "whole track" data were recorded during the early years of the JWRFMP.

2.2 Surfaces Evaluated

2.2.1 Surfaces Evaluated

The search wizard in the database [1] allows the user to specify various combinations of base and surface conditions. See Figure 2.1. Efforts were made to select the same surfaces given in the AIP [2] (Figure 2.2) to the extent possible. The surfaces evaluated are listed in Table 2.1.

🗃 Search Page 3 of 7 🛛 📃 🖂 🖂
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Select Surface Type
Test Base Type:
Pavement 🔽 Ice 🗹 Mixed Conditions
Compacted Snow 🔽 Rough Ice Deselect All
Test Surface condition:
🔽 Drifting Snow 🗹 Dry 🔽 Damp 🔽 Loose blown snow
🔽 Loose Snow 🔽 Slush 🔽 Wet 🔽 Damp/Moist/Frost
Light Snow Mixed Deselect All
Maintenance Action:
🔽 Sand 🛛 🔽 De-Icing Chemical 🔽 None 🗹 Sand and De-Icing
Depth of Contaminant: mm and: mm
Cancel Back Next
Page Navigator
Year and Site Test Type Test Vehicle
Test Speed Time Interval File Format

Figure 2.1: Selectable Base and Surface Conditions in the Database Search Wizard [1]



RUNWAY SURFACE CONDITION (RSC) AND CRFI EQUIVILENT

Figure 2.2: CRFIs Given in the AIP for Various Surfaces [2]

Surface	ERD	TC SFT'79 – all Cs ¹	TC SFT'79 – C3 ¹	IMAG – All Cs ¹	IMAG C3C7 ¹
Bare Ice:		$\sqrt{\frac{1}{\sqrt{2}}}$	√	 √	$\frac{\partial}{\sqrt{\partial t}}$
• >= 0°C					
• 0°C to -10°C					
• <= -10°C					
Bare Ice and Rough Ice:			\checkmark		
• >= 0°C					
• 0°C to -10°C					
• <= -10°C					
Sanded Bare Ice:			\checkmark	\checkmark	
• >= 0°C					
• 0°C to -10°C					
• <= -10°C					
Sanded Bare Ice and			No data	\checkmark	
Rough Ice:					
• >= 0°C					
• 0°C to -10°C					
• <= -10°C					
Bare Packed Snow:					
• > -15°C					
• <= -15°C					
Snow on Pavement:	\checkmark		\checkmark	\checkmark	
• >= 0°C					
• 0°C to -10°C					
• <= -10°C					
Snow on Ice:					
• >= 0°C					
• 0°C to -10°C					
• <= -10°C					
Snow on Rough Ice:			\checkmark		
• >= 0°C					
• 0°C to -10°C					
• <= -10°C	,				
Snow on Packed Snow:	\checkmark	\checkmark	\checkmark	\checkmark	
• >-15°C					
• <= -15°C		,		1	
Bare Pavement		ν	ν	N	
Wet or Damp Pavement:	1		1		I
Wet Pavement	N		N		\mathcal{N}
Damp Pavement	N	1	1	1	1
Slush on any base	$^{\vee}$	\checkmark	\checkmark	\checkmark	

Table 2.1: Database Search Summary

1: Legend (See Table 2.2 for a description of the configurations below):

- TC SFT'79 all Cs: all configurations for the TC SFT'79
- TC SFT'79 C3: configuration 3 for the TC SFT'79
- IMAG all Cs: all configurations for the IMAG
- IMAG C3C7: configurations 3 and 7 for the IMAG

2.2.2 Effect of Snow Depth

The friction coefficients for snow-covered surfaces were also evaluated, although these are not included in the AIP guideline (Figure 2.2). It is well known that snow depth affects measured friction coefficients. Consequently, the effect of snow depth was investigated to assess the most appropriate way to partition the data set.

The effect of snow depth is shown in Figures 2.3 to 2.9 for the devices evaluated. The devices that were evaluated and corresponding configurations are described in section 2.3.



Figure 2.3: Effect of Snow Depth on ERD Readings



Figure 2.4: Effect of Snow Depth on TC SFT'79 Readings (All Configurations)



Figure 2.5: Effect of Snow Depth on TC SFT'79 Readings (Configuration 3)



Figure 2.6: Effect of Snow Depth on IMAG Force Readings (All Configurations)



Figure 2.7: Effect of Snow Depth on IMAG Torque Readings (All Configurations)



Figure 2.8: Effect of Snow Depth on IMAG Force Readings (Configurations 3 and 7)



Figure 2.9: Effect of Snow Depth on IMAG Torque Readings (Configurations 3 and 7)

The effect of snow depth depends on the device and surface under consideration as summarized below:

- (1) ERD (shown in Figure 2.3)
 - a. Snow on Ice Although the relationship is scattered, the ERD reading tends to increase with increasing snow depth. This probably reflects an increasing amount of contaminant drag as the snow depth is increased.
 - b. Snow on Packed Snow Only a few data points are available, which makes it difficult to define trends.
 - c. Snow on Pavement The ERD reading tends to level off (thus becoming independent of snow depth) at depths exceeding 10-20 mm. At lower snow depths, the ERD reading varies significantly from values near those expected for bare pavement to those expected for bare packed snow. This range may reflect differences in snow coverage over the pavement. Alternatively, it may indicate that the vehicle wheels were breaking through the snow cover to reach bare pavement during friction measurements.
- (2) TC SFT'79 (shown in Figures 2.4 and 2.5)
 - a. Snow on Ice Although the relationship is scattered, the friction coefficient tends to increase with increasing snow depth. This probably reflects an increasing amount of contaminant drag as the snow depth is increased.

- b. Snow on Packed Snow The friction coefficient tends to decrease with increasing snow depth for both cases evaluated (i.e., all configurations of the TC SFT'79, and only configuration 3). This trend may reflect increased bonding between the snow on the surface to the packed snow base for deeper depths, which would cause the TC SFT'79 to tend to see a snow surface at deeper snow depths.
- c. Snow on Pavement The TC SFT'79 reading decreases exponentially as the snow depth is increased. As for the "snow on packed snow" case above, this trend may reflect increased bonding between the snow on the surface to the pavement base for deeper depths. This would cause the TC SFT'79 to tend to see a snow surface at deeper snow depths.
- (3) IMAG (shown in Figures 2.6 to 2.9)
 - a. Snow on Ice As for the ERD and the TC SFT'79, the friction coefficient tends to increase with increasing snow depth. This probably reflects an increasing amount of contaminant drag as the snow depth is increased.
 - b. Snow on Packed Snow Only a few data are available, which makes it difficult to identify trends. However, the data tend to indicate that the friction coefficient does not change greatly with increasing snow depth.
 - c. Snow on Pavement As for the TC SFT'79, the IMAG reading decreases exponentially as the snow depth is increased. As for the "snow on packed snow" case above, this trend may reflect increased bonding between the snow on the surface to the pavement base for deeper depths. This would cause the IMAG to tend to see a snow surface at deeper snow depths.

In conclusion, it is evident that all three devices exhibited different trends depending on the surface being considered. This makes it difficult to identify a cut-off snow depth below which the readings were not affected significantly. To allow the analyses to proceed, two cases were analyzed:

- (a) All snow depths
- (b) Snow depths of 10 mm or less

These two snow depth cases were analyzed partly because the size of the data set was quite small for snow depths of 10 mm or less. Often, snow depth data were not available for various sets of friction data (although general surface classifications were available), which necessitated these data sets being eliminated from the data subset being analyzed.

The "all snow depths" case includes data for snow depths exceeding 25 mm (1 inch). See Figures 2.3 to 2.9. It is noted that Transport Canada advises that CRFIs not be taken in snow exceeding this depth. It would be useful to further partition the data set to remove the friction values for snow depths exceeding 25 mm (1 inch).

2.3 Friction Measuring Devices Analyzed

Friction coefficients were evaluated in this project for the following devices:

(1) The ERD

- (2) The TC SFT'79 Two cases were analyzed as follows:
 - All configurations (Table 2.2) It should be noted that two of the configurations apply to the case where the self-wetting system is on (i.e., configurations 5 and 6 Table 2.2). Data for these configurations were not included in the results presented here as these configurations would not be used in wintertime conditions. However, the data for these configurations were included in the overall data quantity evaluations that were made (section 2.4).
 - b. Configuration 3 (Table 2.2) This configuration was evaluated separately as it was the most common one used during the JWRFMP.
- (3) The IMAG Two cases were analyzed as follows:
 - a. All configurations (Table 2.2)
 - b. Configurations 3 and 7 (Table 2.2) These two configurations were evaluated separately as they were the most common ones used during the JWRFMP.

Device	Config'n	Tire Type	Inflation Press (kPa)	Vertical Load (kN)	Slip Ratio (%)	Self- Wetting On?
TC SFT '79 1 ASTM E1551 Ribbed		210	1400	12	no	
TC SFT '79 2 ASTM E1551 Ribbed		690	1400	12	no	
TC SFT '79 3 ASTM E1551 Smooth		690	1400	12	no	
TC SFT '79	4	AERO Smooth Tread	690	1400	12	no
TC SFT '79	5	ASTM E1551 Smooth Tread	690	1400	12	yes
TC SFT '79	6	AERO Smooth Tread	690	1400	12	yes
TC SFT '79	7	ASTM E1551 Ribbed	690	1400	12	no
IMAG	1	PIARC Smooth	150	1800	20	no
IMAG	2	PIARC Smooth	150	1800	5	no
IMAG	3	PIARC Smooth	150	1800	15	no
IMAG	4	PIARC Smooth	150	1800	12	no
IMAG	5	PIARC Smooth	150	1800	50	no
IMAG	6	PIARC Smooth	150	1800	10	no
IMAG	7	PIARC Smooth	165	1800	15	no
IMAG	8	PIARC Smooth	150	1800	15	no
IMAG	9	PIARC Smooth	150	1800	0	no
IMAG	10	PIARC Smooth (note)	165	1800	15	no
IMAG	11	PIARC Smooth	165	1800	30	no
IMAG	12	PIARC Smooth	165	1800	45	no
IMAG	13	PIARC Smooth	165	1800	60	no
IMAG	14	PIARC Smooth	165	1800	75	no
IMAG	15	PIARC Smooth	150	1800	30	no
IMAG	16	PIARC Smooth	150	1800	60	no
IMAG	17	PIARC Smooth	150	1800	90	no
IMAG	18	PIARC Smooth	150	1800	40	no

Table 2.2: List of Configurations

NOTE: Swapped tires with IRV

2.4 Number of Records

The number of records was checked at the start of the work as this provides an indication of the strength of the conclusions that may be obtained from various analyses. The total number of records for all surfaces and cases was 884, 1029, 938, and 1151 for the ERD, TC SFT'79, IMAG Force, and IMAG Torque, respectively. As expected, the number of records was reduced as the data set was partitioned. See Tables 2.3 to 2.5.

Configuration	Year and	Time	Speed ²		Surface I	Track	Number of		
Number ¹	Site	Interval ²		Base	Surface	Depth ²	Maintenance	Section	Data Points
							Action		
All	All	Blank	Blank	All	All	Blank	None	Whole	884
All	All	Blank	Blank	Ice	All	Blank	None	Whole	328
All	All	Blank	Blank	Ice and	All	Blank	None	Whole	408
				Rough Ice					
All	All	Blank	Blank	Ice	Dry	Blank	None	Whole	196
All	All	Blank	Blank	Ice and	Dry	Blank	None	Whole	239
				Rough Ice					
All	All	Blank	Blank	Packed Snow	All	Blank	None	Whole	223
All	All	Blank	Blank	Packed Snow	Dry	Blank	None	Whole	186
All	All	Blank	Blank	Pavement	All	Blank	None	Whole	183
All	All	Blank	Blank	Pavement	Dry	Blank	None	Whole	13

Table 2.3:	Data Q	Juantities a	ind Break	kdown for	the ERD
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Notes:

1. The ERD only has one configuration.

2. By leaving this field blank, the program will include all data.

Configuration	Year and	Time	Speed ¹		Surface	Track	Number of		
Number	Site	Interval ¹	-	Base	Surface	Depth ¹	Maintenance	Section	Data Points
						_	Action		
All^2	All	Blank	Blank	All	All	Blank	None	Whole	1029
All^2	All	Blank	Blank	Ice	All	Blank	None	Whole	390
All^2	All	Blank	Blank	Ice and	All	Blank	None	Whole	465
				Rough Ice					
All^2	All	Blank	Blank	Ice	Dry	Blank	None	Whole	212
All^2	All	Blank	Blank	Ice and	Dry	Blank	None	Whole	226
				Rough Ice					
All^2	All	Blank	Blank	Packed	All	Blank	None	Whole	258
				Snow					
All^2	All	Blank	Blank	Packed	Dry	Blank	None	Whole	191
				Snow					
All^2	All	Blank	Blank	Pavement	All	Blank	None	Whole	249
All^2	All	Blank	Blank	Pavement	Dry	Blank	None	Whole	79
3	All	Blank	Blank	All	All	Blank	None	Whole	760
3	All	Blank	Blank	Ice	All	Blank	None	Whole	314
3	All	Blank	Blank	Ice and	All	Blank	None	Whole	381
				Rough Ice					
3	All	Blank	Blank	Ice	Dry	Blank	None	Whole	174
3	All	Blank	Blank	Ice and	Dry	Blank	None	Whole	188
				Rough Ice	-				
3	All	Blank	Blank	Packed	All	Blank	None	Whole	214
				Snow					
3	All	Blank	Blank	Packed	Dry	Blank	None	Whole	151
				Snow	-				
3	All	Blank	Blank	Pavement	All	Blank	None	Whole	131
3	All	Blank	Blank	Pavement	Drv	Blank	None	Whole	24

Table 2.4: Data Quantities and Breakdown for the TC SFT'79

Notes:

1. By leaving this field blank, the database search wizard will include all data.

2. These data quantities include the data for configurations 5 and 6, which are the ones with the self-wetting system on (Table 2.2). However, the friction data for configurations 5 and 6 were not included in the results presented in section 3 for "all configurations" of the TC SFT'79.

				Surface Parameters					Number of Points
Configuration	Year and	Time	Speed ¹	Base	Surface	Depth ¹	Maintenance	Track	(IMAG Force/IMAG
Number	Site	Interval ¹					Action	Section	Torque)
All	All	Blank	Blank	All	All	Blank	None	Whole	938/1151
All	All	Blank	Blank	Ice	All	Blank	None	Whole	372/448
All	All	Blank	Blank	Ice and	All	Blank	None	Whole	460/562
				Rough					
				Ice					
All	All	Blank	Blank	Ice	Dry	Blank	None	Whole	211/247
All	All	Blank	Blank	Ice and	Dry	Blank	None	Whole	254/298
				Rough					
				Ice					
All	All	Blank	Blank	Packed	All	Blank	None	Whole	218/253
				Snow					
All	All	Blank	Blank	Packed	Dry	Blank	None	Whole	158/189
				Snow					
All	All	Blank	Blank	Pavement	All	Blank	None	Whole	215/265
All	All	Blank	Blank	Pavement	Dry	Blank	None	Whole	46/48
3 and 7	All	Blank	Blank	All	All	Blank	None	Whole	881/1082
3 and 7	All	Blank	Blank	Ice	All	Blank	None	Whole	331/407
3 and 7	All	Blank	Blank	Ice and	All	Blank	None	Whole	413/515
				Rough					
				Ice					
3 and 7	All	Blank	Blank	Ice	Dry	Blank	None	Whole	174/210
3 and 7	All	Blank	Blank	Ice and	Dry	Blank	None	Whole	211/255
				Rough					
				Ice					
3 and 7	All	Blank	Blank	Packed	All	Blank	None	Whole	208/235
				Snow					
3 and 7	All	Blank	Blank	Packed	Dry	Blank	None	Whole	148/171
				Snow					
3 and 7	All	Blank	Blank	Pavement	All	Blank	None	Whole	215/261
3 and 7	All	Blank	Blank	Pavement	Dry	Blank	None	Whole	46/48

Table 2.5: Data Quantities and Breakdown for the IMAG

Notes:

1. By leaving this field blank, the database search wizard will include all data.

3. ANALYSES FOR INDIVIDUAL SURFACES

3.1 Surfaces Quantified in the AIP

The analyses were focused on the surfaces given in the AIP [2], as it is of interest to compare the friction coefficients measured during the JWRFMP with the CRFIs given in the AIP.



RUNWAY SURFACE CONDITION (RSC) AND CRFI EQUIVILENT

Summary results are presented in Figures 3.7 to 3.22. It should be noted that, for formatting reasons, all remaining figures associated with section 3 are presented at the end of section 3.

3.2 Bare Ice and Bare Packed Snow

3.2.1 Bare Ice

Figures 3.7 and 3.8 provide summary results for bare ice not including and including rough ice. Summary results are tabulated in Table 3.1. Detailed results are plotted in Appendix A.

The following observations can be made:

- (1) Comparison to AIP
 - a. Friction coefficients at or above $0^{\circ}C$ The AIP suggests values that tend to be lower than those measured by the devices.
 - b. Friction coefficients below -10°C The values suggested by the AIP are in reasonable agreement with the means measured by the devices.
 - c. Overall comparison The ranges of values suggested by the AIP tend to be smaller than those measured by the devices. In almost all cases, the devices measured values that were both lower than and higher than the lower-bound and upper-bound values suggested by the AIP, respectively.
- (2) Effect of Including or Not Including Rough Ice Data As expected, the inclusion of the rough ice data causes an increase in friction coefficient. However, the increase is relatively

slight, in relation to the overall variation between the maximum and minimum values recorded. Consequently, the conclusions drawn from the analyses will not be affected greatly by whether the rough ice data are included.

This result may be partly due to the fact that the quantity of rough ice data is relatively small compared to that for the smooth ice data. This will cause the friction statistics to be controlled by the smooth ice data.

- (3) Effect of Surface Temperature The friction coefficients measured by each of the devices were not greatly affected by the surface temperature (Appendix A.2).
- 3.2.2 Bare Packed Snow

Figure 3.9 shows summary results for bare packed snow. Summary results are tabulated in Table 3.2. Detailed results are plotted in Appendix B.

The following observations can be made:

- [1] Comparison to AIP
 - a. Friction coefficient below -15°C: All of the friction coefficients measured by the devices were substantially less than the values given in the AIP.
 - b. Friction coefficient above -15°C: The friction coefficients measured by all of the devices were in general agreement with the range of values in the AIP.
 - c. Ranges of friction coefficients: The devices measured a much wider range of friction factors than that given in the AIP.
- [2] Effect of Surface Temperature Typically, there are many more data for surface temperatures above -15°C than below it (Table 3.2), which makes it difficult to infer trends from the summary values listed in Table 3.2. Consequently, the trend plots presented in Appendix B.2 were used to assess the significance of surface temperature. The friction coefficients measured by each of the devices were not greatly affected by the surface temperature (Appendix B.2).
| Device | | Not I | ncluding Roug | h Ice | | | Including Re | ough Ice | |
|------------------|-------------|----------|---|----------|-----------|--------------|----------------|----------|-----------|
| ERD | | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps |
| | mean | 0.12 | 0.111506849 | 0.2 | 0.119439 | 0.131818 | 0.112440476 | 0.19125 | 0.12364 |
| | st dev | 0.039441 | 0.046321104 | 0.132212 | 0.054448 | 0.045318 | 0.04404335 | 0.111411 | 0.052914 |
| | maximum | 0.21 | 0.289999992 | 0.45 | 0.45 | 0.24 | 0.289999992 | 0.45 | 0.45 |
| | minimum | 0.08 | 0.05000001 | 0.08 | 0.05 | 0.08 | 0.050000001 | 0.1 | 0.05 |
| | no of obs | 10 | 146 | 6 | 196 | 22 | 168 | 8 | 239 |
| | | | | | | | | | |
| TC SFT'79 | - | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps |
| (All | mean | 0.183333 | 0.128797468 | 0.097273 | 0.138624 | 0.178571 | 0.129127517 | 0.101667 | 0.139956 |
| Configs) | st dev | 0.060625 | 0.057621183 | 0.031966 | 0.067071 | 0.057652 | 0.05883937 | 0.029951 | 0.067201 |
| | maximum | 0.28 | 0.289999992 | 0.14 | 0.42 | 0.28 | 0.289999992 | 0.16 | 0.42 |
| | minimum | 0.05 | 0.029999999 | 0.05 | 0.03 | 0.05 | 0.029999999 | 0.05 | 0.03 |
| | no of obs | 24 | 158 | 11 | 218 | 28 | 149 | 18 | 226 |
| TC SFT'79 | <u> </u> | <=-10°C | <0°€ to >-10°€ | >= 0°C | All Temps |
~=-10°C | <0°€ to >-10°€ | >= 0°C | All Temps |
| (Config 3) | mean | 0 175625 | 0.1225 | No Data | 0 132126 | 0.18 | 0 12337931 | 0.09 | 0 133351 |
| (0011119 0) | st dev | 0.029205 | 0.055587768 | No Data | 0.062432 | 0.024202 | 0.055417865 | No data | 0.062454 |
| | maximum | 0.020200 | 0.2899999992 | 0 | 0.002 102 | 0.21 | 0.2899999992 | 0.09 | 0.002 101 |
| | minimum | 0.11 | 0.0299999999 | 0 | 0.03 | 0.13 | 0.0299999999 | 0.09 | 0.03 |
| | no of obs | 16 | 136 | 0 | 174 | 15 | 145 | 1 | 188 |
| | 10 01 2.2.2 | | | | | | | | |
| IMAG | | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps |
| Force | mean | 0.237667 | 0.184367816 | No Data | 0.203415 | 0.260204 | 0.196111111 | 0.21 | 0.215645 |
| (All | st dev | 0.033803 | 0.041699398 | No Data | 0.052758 | 0.042793 | 0.045980877 | No data | 0.056565 |
| Configs) | maximum | 0.3 | 0.319999993 | 0 | 0.4 | 0.34 | 0.319999993 | 0.21 | 0.4 |
| , se s | minimum | 0.17 | 0.09000004 | 0 | 0.09 | 0.17 | 0.109999999 | 0.21 | 0.09 |
| | no of obs | 30 | 87 | 0 | 205 | 49 | 72 | 1 | 248 |
| | | | | | | | | | |
| IMAG | | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps |
| Torque | mean | 0.155238 | 0.151214954 | 0.114 | 0.146166 |
0.165652 | 0.153200001 | 0.165652 | 0.150625 |
| (All | st dev | 0.034587 | 0.038820104 | 0.014298 | 0.053049 |
0.034406 | 0.04014821 | 0.128446 | 0.050515 |
| Configs) | maximum | 0.22 | 0.25999999 | 0.14 | 0.68 |
0.23 | 0.25999999 | 0.68 | 0.68 |
| | minimum | 0.07 | 0.07 | 0.1 | 0.07 | 0.07 | 0.07 | 0.1 | 0.07 |
| | no of obs | 42 | 107 | 10 | 253 | 69 | 100 | 23 | 304 |
| | | | | | | | | | |
| IMAG | | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps | <=-10°C | <0°C to >-10°C | >= 0°C | All Temps |
| Force | mean | 0.235 | 0.18654321 | 0.168 | 0.205238 | 0.258919 | 0.191744186 | 0.14 | 0.217463 |
| (Configs | st dev | 0.0373 | 0.040686621 | 0.040249 | 0.045068 | 0.048177 | 0.043876615 | 0.014142 | 0.050627 |
| 3 & 7) | maximum | 0.3 | 0.319999993 | 0.21 | 0.37 |
0.34 | 0.319999993 | 0.16 | 0.37 |
| | minimum | 0.17 | 0.109999999 | 0.13 | 0.11 | 0.17 | 0.109999999 | 0.13 | 0.11 |
| | no of obs | 24 | 81 | 5 | 168 | 37 | 86 | 4 | 205 |
| IMAG | <u> </u> | <- 10°C | <0°C to > 10°C | >= 0°C | | <- 10°C | <0°C to >_10°C | >= 0°C | |
| | mean | < -10 C | 0 152475248 | 2=0.0 | 0 1/0250 | 0 165614 | 0 153867025 | 0 171875 | All Temps |
| (Configs | st dev | 0.137714 | 0.132473240 | 0.172941 | 0.054894 | 0.103014 | 0.133007923 | 0.171073 | 0.155210 |
| (00mg3
3 & 7) | maximum | 0.004733 | 0.0000000000000000000000000000000000000 | 0.140400 | 0.00-000 | 0.00710 | 0.0000000000 | 0.104719 | 0.001001 |
| 0 4 1) | minimum | 0.22 | 0.079999998 | 0.00 | 0.00 | 0.20 | 0.079999998 | 0.00 | 0.00 |
| | no of obs | 35 | 101 | 17 | 216 | 57 | 106 | 16 | 261 |

Table 3.1: Summary Results for Bare Ice

Device		Friction Coefficient by Temperature							
ERD		<=-15°C	>-15°C	All Temperatures					
	mean	0.2875	0.184638	0.198817205					
	st dev	0.005	0.063501	0.066346338					
	maximum	0.29	0.63	0.629999995					
	minimum	0.28	0.09	0.090000004					
	no of obs	4	138	186					
TC SFT'79		<=-15°C	>-15°C	All Temperatures					
(All	mean	0.239375	0.219478	0.226073298					
Configs)	st dev	0.045088	0.038202	0.042436019					
	maximum	0.29	0.35	0.349999994					
	minimum	0.16	0.13	0.119999997					
	no of obs	16	115	191					
			-						
TC SFT'79	•	<=-15°C	>-15°C	All Temperatures					
(Config 3)	mean	No Data	0.219333	0.227483444					
	st dev	No Data	0.029622	0.042758525					
	maximum	0	0.33	0.349999994					
	minimum	0	0.14	0.119999997					
	no of obs	0	105	151					
		1 = 2 0	4.50.0	A 11 - T					
IMAG		<=-15°C	>-15°C	All Temperatures					
Force	mean	0.275714	0.250851	0.263903449					
(All	st dev	0.019101	0.054054	0.053789886					
Configs)	maximum	0.3	0.37	0.372999996					
	minimum	0.25	0.15	0.150000006					
	no of obs	14	94	145					
		1 1500	. 15%						
Torquo	maan	0.10	>-10 0						
	niean st dov	0.10	0.183511	0.109100310					
(All Configs)		0.021034	0.040704	0.042400004					
Conings)	minimum	0.22	0.31	0.310000002					
	no of obs	0.14	131	0.10000001					
			101	202					
IMAG		<=-15°€	>-15°C	All Temperatures					
Force	mean	0.28375	0.251429	0.265525927					
(Configs	st dev	0.020659	0.054845	0.05479471					
3 & 7)	maximum	0.3	0.37	0.372999996					
,	minimum	0.25	0.15	0.150000006					
	no of obs	8	91	135					
IMAG	-	<=-15°C	>-15°C	All Temperatures					
Torque	mean	0.1792	0.183171	0.190391305					
(Configs	st dev	0.023965	0.041038	0.043324031					
3 & 7)	maximum	0.23	0.31	0.31000002					
	minimum	0.14	0.1	0.10000001					
	no of obs	25	123	184					

 Table 3.2: Summary Results for Bare Packed Snow

3.3 Sanded Ice

Figures 3.10 and 3.11 provide summary results for bare ice not including and including rough ice. Summary results are tabulated in Table 3.3. Detailed results are plotted in Appendix C.

The data set for sanded ice is quite small (Table 3.3), which limits the strength of the conclusions that can be drawn. Nevertheless, the following preliminary observations can be made:

- (1) Comparison to AIP The measured friction coefficients span a much wider range of values than that given in the AIP.
- (2) Comparison to Un-Sanded Ice The friction coefficients for sanded ice tend to be higher than those for un-sanded ice.
- (3) Effect of Including or Not Including Rough Ice Data This had no significant effect.
- (4) Effect of Surface Temperature The friction coefficient was not greatly affected by the surface temperature (Appendix C.1).

3.4 Snow on Ice, Pavement and Packed Snow

3.4.1 Snow-Covered Ice

Figures 3.12 and 3.13 provide summary results for snow-covered ice (not including rough ice) for all snow depths, and for snow depths of 10 mm or less, respectively. Figures 3.14 and 3.15 provide summary results for bare ice (including rough ice) for all snow depths, and for snow depths of 10 mm or less, respectively. Summary results are tabulated in Tables 3.4 and 3.5 for bare ice not including and including rough ice, respectively. Detailed results are plotted in Appendix E.

The following observations can be made:

- (1) Comparison to AIP Comparisons are not possible because this case is not covered by the AIP.
- (2) Effect of Including or Not Including Rough Ice Data This did not affect the conclusions significantly due to the large ranges of variation that were measured.
- (3) Effect of Including All Snow Depths vs. Limiting the Analyses to Snow Depths of 10 mm or Less – Wider ranges of variation were observed for the full data set. However, the mean friction coefficients were generally similar for each case.
- (4) Effect of Surface Temperature The trends for the whole data set were highly scattered (Appendix D.2), which is partly due to the fact that all snow depths were mixed. However, the plots produced for the data subset with snow depths of 10 mm or less were also scattered (Appendix E.5), which indicates that the friction coefficients were not greatly affected by the surface temperature.

ERD <=-10°C	Device		Sand	ed Ice Not Incl	uding Rou	gh Ice	Sa	nded Ice Includ	ing Rough	lce
mean 0.3 0.281033331 0.23 0.24167 0.021111 0.25245714 0.023 0.24167 st dev No Data 0.02915735 No Data 0.061788 No Data 0.046368 maximum 0.3 0.34000004 0.23 0.34 0.3 0.34000004 0.23 0.16 more of obs 1 12 9 7 1 24 TC SFT79 <=-10°C	ERD		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
stdev No Data 0.092915735 No Data 0.051316 0.038873 0.06738816 No Data 0.046386 minimum 0.3 0.340000004 0.23 0.34 0.3 0.340000004 0.23 0.34 minimum 0.3 0.159999996 0.23 0.16 0.17 0.159999996 0.23 0.16 more dots 1 3 1 12 9 7 1 24 CSTPT9 <=10°C		mean	0.3	0.263333331	0.23	0.241667	0.221111	0.254285714	0.23	0.2325
maximum 0.3 0.340000004 0.23 0.34 0.3 0.340000004 0.23 0.13 Inio of obs 1 3 1 12 9 7 1 24 TC SFT79 <=-10°C		st dev	No Data	0.092915735	No Data	0.051316	0.038873	0.067788186	No Data	0.046368
minimum 0.3 0.159999996 0.23 0.16 0.17 0.159999996 0.23 0.16 TC SFT79 <=-10°C		maximum	0.3	0.340000004	0.23	0.34	0.3	0.340000004	0.23	0.34
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		minimum	0.3	0.159999996	0.23	0.16	0.17	0.159999996	0.23	0.16
CSFT"9 <=-10°C <0°C All Temps <=-10°C <0°C All Temps (All mean No Data 0.636666665 0.11 0.426 No Data 0.636666665 0.11 0.426 Configs) si dev No Data 0.073936908 0.040625 0.278466 No Data 0.63999988 0.17 0.7 minimum 0 0.59999988 0.17 0.7 0 0.69999988 0.17 0.7 minimum 0 0.59999988 0.17 0.7 0 0.69999988 0.17 0.7 Configs) mean No Data 0.63666665 No Data 0.63666667 No Data 0.63666665 No Data 0.63666665 No Data 0.073937 No Data 0.073936908 No Data 0.073936908 No Data 0.073937 No Data 0.63666665 No Data 0.6366665 No Data 0.63666662 No Data 0.63666662 No Data 0.63666662 No Data 0.63666662 No Data 0.656666667 0.0265 <td></td> <td>no of obs</td> <td>1</td> <td>3</td> <td>1</td> <td>12</td> <td>9</td> <td>7</td> <td>1</td> <td>24</td>		no of obs	1	3	1	12	9	7	1	24
TC SFT79 <=-10°C <0°C to >-10°C >= 0°C All Temps <=-10°C <0°C to >-10°C >= 0°C All Temps (All Configs) mean No Data 0.073936908 0.040825 0.278496 No Data 0.073936908 0.040825 0.278496 maximum 0 0.69999988 0.17 0.7 0 0.689999988 0.17 0.7 minimum 0 0.5 0.08 0.08 0 6 4 10 TC SFT79 <=-10°C										
(All Configs) mean intimum No Data 0 0.636666665 0.011 0.426 0.04825 No Data 0.278496 No Data 0.6396999988 0.17 0.7 minimum 0 0.699999988 0.17 0.7 0 0.639999988 0.17 0.7 mo of obs 0 6 4 10 0 6 4 10 TC SFT79 <=10°C	TC SFT'79		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
Configs) st dev No Data 0.073936908 0.040825 0.278496 No Data 0.073936908 0.040825 0.278496 maximum 0 0.69999988 0.17 0.7 0 0.69999988 0.17 0.7 more of obs 0 6 4 10 0 6 4 10 TC SFT79 <=-10°C	(All	mean	No Data	0.636666665	0.11	0.426	No Data	0.636666665	0.11	0.426
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Configs)	st dev	No Data	0.073936908	0.040825	0.278496	No Data	0.073936908	0.040825	0.278496
minimum 0 0.5 0.08 0.0 0.5 0.08 0.0 TC SFT79 <=-10°C		maximum	0	0.699999988	0.17	0.7	0	0.699999988	0.17	0.7
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		minimum	0	0.5	0.08	0.08	0	0.5	0.08	0.08
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		no of obs	0	6	4	10	0	6	4	10
Inc Sin 7 is (Config 3) mean st dev No Data 0.0366666650 No Data 0.0366666650 No Data 0.0366666650 No Data 0.03666666650 No Data 0.03666670 No Data 0.036666666650 No Data 0.03666670 No Data 0.03666670 No Data 0.03666670 No Data 0.0366670 No Data 0.03525 0.0556666620 No Data 0.0411 Temps MAG <=-10°C			<i>4</i> − 10°C	<0°C to > 10°C	>_ 0°C	All Tompo	- 10°C	<0°C to > 10°C	> – 0°C	
Interim No Data 0.030000000000000000000000000000000000	(Config 2)	moon	<=-10 C		>= 0 C		<=-10 C		>= 0 C	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	(Coning 3)	niean et dou	No Data	0.030000000	No Data	0.030007	No Data	0.030000000	No Data	0.030007
Intakinum 0 0.09999998 0 0.7 0 0 0.09999998 0 0.7 0 <t< td=""><td></td><td></td><td>NO Dala</td><td>0.073930908</td><td>NU Dala</td><td>0.073937</td><td></td><td>0.073930908</td><td></td><td>0.073937</td></t<>			NO Dala	0.073930908	NU Dala	0.073937		0.073930908		0.073937
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		minimum	0	0.0999999966	0	0.7	0	0.0999999900	0	0.7
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			0	0.3	0	0.5	0	0.5	0	0.5
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			0	0	0	0	0	0	0	0
mean No Data 0.080591669 No Data 0.050666622 No Data 0.089591669 No Data 0.089591669 No Data 0.044 (All st dev No Data 0.089591669 No Data 0.089591669 No Data 0.120384 Configs) maximum 0 0.639999986 0 0.64 0.39 0.639999986 0 0.64 IMAG c=-10°C <0°C to >-10°C 0.419999987 0 0.42 0.31 0.419999987 0 0.31 IMAG <=-10°C	IMAG		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
No.cor No.cor No.cor No.cor No.cor State No.cor Configs is dev No.cor 0.639999986 0 0.027646 0.089591669 No.cor 0.639999986 0 0.64 IMAG 0.039591669 No.cor 0 0.419999987 0 0.42 0.31 0.419999987 0 0.31 IMAG - - - - - - - - - - - 0 0.31 0.419999987 0 0.42 0.31 0.419999987 0 0.31 IMAG - - - - - - - - - - 0 0.31 Configs) mean No Data 0.49666667 0.2075 0.381 0.24625 0.29208335 0.281 0.281 0.157 Configs) maximum 0 0.57999983 0.28 0.58 0.28 0.579999983 0.28 0.58 <td>Force</td> <td>mean</td> <td>No Data</td> <td>0 556666666</td> <td>No Data</td> <td>0 556667</td> <td>0.3525</td> <td>0 556666662</td> <td>No Data</td> <td>0.44</td>	Force	mean	No Data	0 556666666	No Data	0 556667	0.3525	0 556666662	No Data	0.44
Configs) maximum 0 0.633999986 0 0.64 0.39 0.633999986 0 0.64 minimum 0 0.419999987 0 0.42 0.31 0.419999987 0 0.31 ino of obs 0 6 0 6 8 6 0 14 IMAG <=-10°C	(All	st dev	No Data	0.089591669	No Data	0.089592	0.027646	0.089591669	No Data	0.120384
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Configs)	maximum	0	0.639999986	0	0.64	0.39	0.639999986	0	0.64
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	g-,	minimum	0	0.419999987	0	0.42	0.31	0.419999987	0	0.31
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		no of obs	0	6	0	6	8	6	0	14
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$										
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	IMAG		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Torque	mean	No Data	0.49666667	0.2075	0.381	0.24625	0.292083335	0.2075	0.2725
Configs maximum 0 0.579999983 0.28 0.58 0.28 0.579999983 0.28 0.58 minimum 0 0.349999994 0.17 0.17 0.21 0.15000006 0.17 0.15 no of obs 0 6 4 10 8 24 4 36 IMAG <=-10°C	(All	st dev	No Data	0.093523619	0.051881	0.167495	0.025036	0.13493893	0.051881	0.115
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Configs)	maximum	0	0.579999983	0.28	0.58	0.28	0.579999983	0.28	0.58
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		minimum	0	0.349999994	0.17	0.17	0.21	0.150000006	0.17	0.15
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		no of obs	0	6	4	10	8	24	4	36
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $										
Force (Configs 3 & 7) mean No Data 0.55666662 #DIV/0! 0.556667 0.3525 0.55666662 No Data 0.44 (Configs 3 & 7) st dev No Data 0.089591669 #DIV/0! 0.089592 0.027646 0.089591669 No Data 0.120384 3 & 7) maximum 0 0.639999986 0 0.64 0.39 0.639999986 0 0.64 minimum 0 0.419999987 0 0.42 0.31 0.419999987 0 0.31 no of obs 0 6 0 6 8 6 0 14 IMAG <=-10°C	IMAG		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
(Configs 3 & 7) st dev No Data 0.089591669 #DIV/0! 0.089592 0.027646 0.089591669 No Data 0.120384 3 & 7) maximum 0 0.639999986 0 0.64 0.39 0.639999986 0 0.64 minimum 0 0.419999987 0 0.42 0.31 0.419999987 0 0.31 no of obs 0 6 0 6 8 6 0 14 IMAG <=-10°C	Force	mean	No Data	0.556666662	#DIV/0!	0.556667	0.3525	0.556666662	No Data	0.44
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	(Configs	st dev	No Data	0.089591669	#DIV/0!	0.089592	0.027646	0.089591669	No Data	0.120384
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	3 & 7)	maximum	0	0.639999986	0	0.64	0.39	0.639999986	0	0.64
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		minimum	0	0.419999987	0	0.42	0.31	0.419999987	0	0.31
IMAG <td></td> <td>no of obs</td> <td>0</td> <td>6</td> <td>0</td> <td>6</td> <td>8</td> <td>6</td> <td>0</td> <td>14</td>		no of obs	0	6	0	6	8	6	0	14
Torque (Configs mean No Data 0.49666667 0.2075 0.381 0.24625 0.292083335 0.2075 0.2725 3 & 7) maximum 0 0.579999983 0.28 0.58 0.28 0.579999983 0.28 0.58 no of obs 0 6 4 10 8 24 4 26	IMAG		< 10°C	$<0^{\circ}$ C to $> 10^{\circ}$ C	>= 0°C		< 10°C	<0°C to > 10°C	>= 0°C	
Integrit No Data 0.49000007 0.2073 0.381 0.24025 0.292083335 0.2073 0.2725 (Configs 3 & 7) st dev No Data 0.093523619 0.051881 0.167495 0.025036 0.13493893 0.051881 0.115 3 & 7) maximum 0 0.579999983 0.28 0.58 0.28 0.579999983 0.28 0.58 minimum 0 0.349999994 0.17 0.17 0.21 0.15000006 0.17 0.15 no of obs 0 6 4 10 8 24 4 26	Torquo	moon	No Data	0 40666667	>= 0 C		0.24625	0 202082225	>= 0 C	
3 & 7) maximum 0 0.579999983 0.28 0.58 0.28 0.579999983 0.28 0.58 no of obs 0 6 4 10 8 24 4 26	Configs	et dov	No Data	0.49000007	0.2075	0.301	0.24023	0.292003333	0.2073	0.2723
maximum 0 0.373333300 0.20 0.30 0.20 0.373333900 0.20 0.3733393900 0.20 0.3733939300 0.20 0.3733939300 0.20 0.3733939300 0.20 0.3733939300 0.20 0.30 0.20 0.3733939300 0.20 0.30 0.20 0.3733939300 0.20 0.30 0.20 0.3733939300 0.20 0.30 0.20 0.30 0.20 0.3733939300 0.20 0.30 0.20 0.3733939300 0.20 0.30 0.20 0.3733939300 0.20 0.30 0.20 0.3733939300 0.20 0.30 0.3733939300 0.20 0.30 0.373393939300 0.20 0.30 0.3733939300 0.20 0.30 0.3733939300 0.20 0.30 0.3733939300 0.20 0.30 0.3733939300 0.20 0.30 0.3733939300 0.20 0.30 0.3733939300 0.30 0.30 0.3733939300 0.30 0.30 0.3733939300 0.30 0.30 0.3733939300 <th0.30< th=""> 0.30 0.3733939300</th0.30<>	3 & 7)	mavimum		0.570000093	0.001001	0.107495	 0.020000	0.13493093	0.001001	0.113
	501)	minimum	0	0.3/9999903	0.20	0.30	 0.20	0.37 9999903	0.20	0.00
		no of obs	0	6.5 4 55555555	0.17	10	 0.21 8	24	0.17	36

Table 3.3: Summary Results for Sanded Ice

Device		Ai	ny Snow Dep	th				Snow Depth	< 10 mm	
ERD		<=-10°C	<0°C to >-10	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
	mean	0.178889	0.17455072	No Data	0.192358		0.24	0.165764706	No Data	0.169889
	st dev	0.05819	0.05930022	No Data	0.073699		0	0.037315249	No Data	0.040128
	maximum	0.24	0.33000001	0	0.39		0.24	0.282999992	0	0.283
	minimum	0.1	0.07	0	0.07		0.24	0.094999999	0	0.095
	no of obs	9	69	0	95		2	34	0	36
TC SFT'79		<=-10°C	<0°C to >-10	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
(All	mean	0.177391	0.1614486	No Data	0.166341		0.166364	0.150121952	No Data	0.153558
Configs)	st dev	0.093479	0.07975792	No Data	0.081864		0.102788	0.056018834	No Data	0.067659
	maximum	0.33	0.37	0	0.37		0.31	0.370000005	0	0.37
	minimum	0.04	0.04	0	0.04		0.04	0.07	0	0.04
	no of obs	23	107	0	138		11	41	0	52
TC SET'70		<−-10°C	<0°C to >-10	<u>>− 0°C</u>			<− - 10°C	<0°C to >-10°C	<u>>− 0°C</u>	
(Config 3)	mean	0.16	0 15716405	No Data	0 15630/		0.16	0 144571420	No Data	0 145780
(Comig 0)	st dev	0.10	0.08041853	No Data	0.077774		0.10	0.058828908	No Data	0.056599
	maximum	0.01	0.000+1000	110 Data	0.07777	_	0.01	0.370000005	110 Data	0.0000000
	minimum	0.17	0.04	0	0.04		0.17	0.07	0	0.07
	no of obs	3	97	0	104		3	35	0	38
					10-1		0		•	
IMAG		<=-10°C	<0°C to >-10	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
Force	mean	0.246333	0.21557895	No Data	0.22296		No Data	0.2033333334	No Data	0.203333
(All	st dev	0.047669	0.07286998	No Data	0.06878		No Data	0.03396831	No Data	0.033968
Configs)	maximum	0.33	0.38	0	0.38		0	0.289999992	0	0.29
0,	minimum	0.18	0.09	0	0.09		0	0.159999996	0	0.16
	no of obs	30	95	0	125		0	27	0	27
IMAG		<=-10°C	<0°C to >-10	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
Torque	mean	0.1638	0.1653271	No Data	0.165217		0.21375	0.172222222	No Data	0.181714
(All	st dev	0.053486	0.06402119	No Data	0.060011		0.035832	0.030801264	No Data	0.036095
Configs)	maximum	0.26	0.31	0	0.31		0.26	0.239999995	0	0.26
	minimum	0.06	0.03	0	0.03		0.15	0.109999999	0	0.11
	no of obs	50	107	0	161		8	27	0	35
IMAG	1	<=-10°C	<0°C to >-10	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
Force	mean	0.253333	0.21553192	No Data	0.223967		0.22	0.202692308	No Data	0.203333
(Configs	st dev	0.045234	0.07325926	No Data	0.06966		No Data	0.03447407	No Data	0.033968
3 & 7)	maximum	0.33	0.38	0	0.38		0.22	0.289999992	0	0.29
	minimum	0.19	0.09	0	0.09		0.22	0.159999996	0	0.16
	no of obs	27	94	0	121		1	26	0	27
IMAG		<=-10°C	<0°C to >-10	>= 0°C	All Temps		<=-10°€	<0°C to >-10°C	>= 0°C	All Temps
Torque	mean	0.167234	0.16584906	No Data	0.166624		0.202222	0.174615385	No Data	0.181714
(Confias	st dev	0.053312	0.06409618	No Data	0.060102		0.048161	0.028737538	No Data	0.036095
3 & 7)	maximum	0.26	0.31	0	0.31		0.26	0.239999995	0	0.26
- ,	minimum	0.06	0.03	0	0.03		0.11	0.140000001	0	0.11
	no of obs	47	106	0	157		9	26	0	35

Table 3.4: Summary Results for Snow-Covered Ice – Not Including Rough Ice

Device		A	Any Snow Dept	h				Snow Depth	< 10 mm	
ERD		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°0	>= 0°C	All Temps
	mean	0.149444	0.180695652	No Data	0.188326		0.253333	0.16910204	No Data	0.173887
	st dev	0.065212	0.058113898	No Data	0.070961		0.023094	0.038762226	No Data	0.042349
	maximum	0.28	0.330000013	0	0.39		0.28	0.282999992	0	0.283
	minimum	0.09	0.07	0	0.07		0.24	0.094999999	0	0.095
	no of obs	18	92	0	129		3	49	0	53
TC SFT'79		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°0	>= 0°C	All Temps
(All	mean	0.191111	0.166007463	0.1025	0.168636		0.194	0.164402986	No Data	0.169817
Configs)	st dev	0.092584	0.076595265	0.023629	0.076791		0.099484	0.059838941	No Data	0.068998
	maximum	0.33	0.370000005	0.12	0.37		0.31	0.370000005	0	0.37
	minimum	0.04	0.039999999	0.07	0.04		0.04	0.07	0	0.04
	no of obs	27	134	4	187	_	15	67	0	82
TC SFT'79		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	\vdash	<=-10°C	<0°C to >-10°0	>= 0°C	All Temps
(Config 3)	mean	0.170714	0.160826772	No Data	0.161069		0.1775	0.1615	No Data	0.1625
(00g 0)	st dev	0.020178	0.076492463	No Data	0.072005		0.03594	0.062309371	No Data	0.060932
	maximum	0.23	0.370000005	0	0.37		0.23	0.370000005	0	0.37
	minimum	0.15	0.039999999	0	0.04		0.15	0.07	0	0.07
	no of obs	14	127	0	145		4	60	0	64
IMAG		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°0	>= 0°C	All Temps
Force	mean	0.250526	0.211491229	No Data	0.222911		No Data	0.198260869	No Data	0.205962
(All	st dev	0.043243	0.06952726	No Data	0.065368		No Data	0.039231751	No Data	0.042898
Configs)	maximum	0.33	0.379999995	0	0.38		0	0.289999992	0	0.29
• /	minimum	0.18	0.09000004	0	0.09		0	0.140000001	0	0.14
	no of obs	38	114	0	158		0	46	0	52
IMAG		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°0	>= 0°C	All Temps
Torque	mean	0.159848	0.16	No Data	0.160991		0.205	0.153913044	No Data	0.16625
(All	st dev	0.055206	0.059603628	No Data	0.056923		0.03451	0.038208682	No Data	0.041077
Configs)	maximum	0.26	0.31000002	0	0.31		0.26	0.239999995	0	0.26
	minimum	0.02	0.029999999	0	0.02		0.15	0.10000001	0	0.1
	no of obs	66	136	0	212		12	46	0	64
IMAG		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps
Force	mean	0.256286	0.21141593	No Data	0.223701		0.22	0.19777778	No Data	0.205962
(Configs	st dev	0.040226	0.06983229	No Data	0.066006		No Data	0.039536453	No Data	0.042898
3 & 7)	maximum	0.33	0.379999995	0	0.38		0.22	0.289999992	0	0.29
	minimum	0.19	0.090000004	0	0.09		0.22	0.140000001	0	0.14
	no of obs	35	113	0	154		1	45	0	52
IMAG		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	\vdash	<=-10°C	<0°C to >-10°0	>= 0°C	All Temps
Torque	mean	0.162222	0.16037037	No Data	0.161971		0.197692	0.154888889	No Data	0.16625
(Configs	st dev	0.055371	0.059668329	No Data	0.057015		0.04226	0.038056311	No Data	0.041077
3 & 7)	maximum	0.26	0.31000002	0	0.31		0.26	0.239999995	0	0.26
,	minimum	0.02	0.029999999	0	0.02		0.11	0.10000001	0	0.1
	no of obs	63	135	0	208		13	45	0	64

Table 3.5: Summary Results for Snow-Covered Ice – Including Rough Ice

3.4.2 Snow-Covered Pavement

Figures 3.16 and 3.17 provide summary results for snow-covered pavement for all snow depths, and for snow depths of 10 mm or less, respectively. Summary results are tabulated in Table 3.6. Detailed results are plotted in Appendix D.

The following observations can be made:

- (1) Comparison to AIP Comparisons are not possible, as the AIP does not provide guideline CRFI values for this case.
- (2) Ranges of Values The measured values span a wide range for each device and each snow depth case analyzed.
- (3) Effect of Limiting the Analyses to Snow Depths of 10 mm or Less The friction coefficients were lower for the "10 mm or Less" case, particularly with respect to mean values.
- (4) Effect of Surface Temperature Typically, there are many more data for surface temperatures in the range of 0°C to -10°C than for the other temperature ranges (Table 3.6), which makes it difficult to infer trends from the summary values listed in Table 3.6. Consequently, the trend plots presented in Appendices D.2 and D.5 were used to assess the significance of surface temperature. The plots are highly scattered for both snow depth cases (Appendices D.2 and D.5), which indicates that the friction coefficients are not strongly related to the surface temperature.

3.4.3 Snow-Covered Packed Snow

Figures 3.18 and 3.19 provide summary results for snow-covered packed snow for all snow depths, and for snow depths of 10 mm or less, respectively. Summary results are tabulated in Table 3.7. Detailed results are plotted in Appendix F.

The following observations can be made:

- (1) Comparison to AIP The measured friction coefficients are in reasonable agreement with the values in the AIP. Furthermore, the ranges of variation are generally similar.
- (2) Effect of Including All Snow Depths vs. Limiting the Analyses to Snow Depths of 10 mm or Less The friction coefficients are lower for the "10 mm or Less" case. As well, the ranges of variation are much smaller than the "10 mm or Less" case.
- (3) Effect of Surface Temperature The plots are quite scattered (Appendices F.2 and F.5), which indicates that the friction coefficients are not greatly affected by the surface temperature.

Device			All Snow I	Depths			Snow Depths of 10 mm or Less				
ERD		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	
	mean	0.298571	0.279827588	0.515	0.306116		0.29	0.294999999	0.515	0.33	
	st dev	0.040591	0.110286571	0.047958	0.10447		#DIV/0!	0.111897504	0.047958	0.130352	
	maximum	0.36	0.660000026	0.58	0.66		0.29	0.649999976	0.58	0.65	
	minimum	0.23	0.140000001	0.47	0.14		0.29	0.140000001	0.47	0.14	
	no of obs	7	58	4	121		1	20	4	25	
				_							
TC SFT'79	-	<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	
(All	mean	0.195833	0.188472223	0.2225	0.171626		0.29	0.263636363	0.2225	0.261667	
Configs)	st dev	0.077748	0.15936193	0.078475	0.131631		0.008165	0.232185178	0.078475	0.200019	
	maximum	0.3	0.730000019	0.3	0.73		0.3	0.730000019	0.3	0.73	
	minimum	0.07	0.01	0.15	0.01		0.28	0.07	0.15	0.07	
	no of obs	12	72	4	123		4	22	4	30	
TC SET 70		< 10°C	<0°C to > 10°C	>= 0°C			< 10°C	$<0^{\circ}$ C to $> 10^{\circ}$ C	>- 0°C		
(Config 2)	moon	<=-10 C	<0 C $10 > 10$ C	>= 0 C			<=-10 C		>= 0 C	All Temps	
(Coning 3)	inean at day	No Data	0.200000001	0.2223	0.17974		No Data	0.210000000	0.2223	0.212727	
			0.136972707	0.076473	0.133315		NU Dala	0.221203071	0.076473	0.201333	
	maximum	0	0.730000019	0.3	0.73		0	0.730000019	0.3	0.73	
	minimum	0	0.01	0.15	0.01		0	0.07	0.15	0.07	
	ado io on	0	48	4	11		0	18	4	22	
IMAG		<10°C	<0°C to >-10°C	<u>>− 0°C</u>	All Temps		<−-10°C	<0°C to >-10°C	>- 0°C		
Force	mean	No Data	0 282753624		0 277944		No Data	0 303448276	2= 0 C	0 203880	
	st dev	No Data	0.202733024	0.203	0.120891		No Data	0.207231336	0.254200	0.233003	
(All	maximum		0.140410100	0.007070	0.120001		110 Data	0.207201000	0.007700	0.100002	
Coningo)	minimum	0	0.140000001	0.04	0.07		0	0.140000001	0.04	0.07	
	no of obs	0	69	10	107		0	29	0.10	36	
		Ŭ		10	107		Ŭ	20	,		
IMAG	•	<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	
Torque	mean	0.161667	0.174731183	0.17	0.163333		0.188333	0.197575756	0.19	0.195217	
(All	st dev	0.048399	0.142756949	0.06532	0.117002		0.031885	0.208851475	0.068557	0.178248	
Configs)	maximum	0.23	0.829999983	0.3	0.83		0.23	0.829999983	0.3	0.83	
0,	minimum	0.08	0.02	0.1	0.02		0.14	0.02	0.1	0.02	
	no of obs	12	93	10	159		6	33	7	46	
IMAG		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps		<=-10°C	<0°C to >-10°C	>= 0°C	All Temps	
Force	mean	No Data	0.282941177	0.265	0.277944		No Data	0.303448276	0.254286	0.293889	
(Configs	st dev	No Data	0.146491899	0.057975	0.120891		No Data	0.207231336	0.067788	0.188502	
3 & 7)	maximum	0	0.870000005	0.34	0.87		0	0.870000005	0.34	0.87	
	minimum	0	0.140000001	0.16	0.14		0	0.140000001	0.16	0.14	
	no of obs	0	68	10	107		0	29	7	36	
		4000			A II		4000			A 11 - T	
IMAG T	1	<=-10°C	$<0^{\circ}C$ to >-10°C	>= 0°C	All Temps		<=-10°C	$<0^{\circ}C$ to $>-10^{\circ}C$	>= 0°C	All Temps	
lorque	mean	0.161667	0.1/4761905	0.17	0.166516	<u> </u>	0.188333	0.219310344	0.19	0.21	
(Configs	st dev	0.048399	0.143941723	0.06532	0.116767		0.031885	0.213974814	0.068557	0.1/9661	
3&1)	maximum	0.23	0.829999983	0.3	0.83		0.23	0.829999983	0.3	0.83	
	minimum	0.08	0.050000001	0.1	0.02		0.14	0.050000001	0.1	0.05	
	no of obs	12	84	10	155	I	6	29	7	42	

Table 3.6: Summary Results for Snow on Pavement

ERD <=-15°C	Device		All	Snow Dep	ths	Snow Dep	nm or Less	
mean No Data 0.20188 0.211481 No Data 0.204051 0.04051 st dev No Data 0.047972 0.047935 No Data 0.04051 0.04051 maximum 0 0.32 0.32 0 0.27 0.27 minimum 0 0.12 0.12 0 0.17 0.17 no of obs 0 22 27 0 8 8 TC SFT79 <=-15°C	ERD		<=-15°C	> -15°C	All Temps	<=-15°C	> -15°C	All Temps
st dev No Data 0.04792 0.047935 No Data 0.040917 0.047 maximum 0 0.12 0.12 0 0.17 0.17 no of obs 0 22 27 0 8 8 TC SFT'79 <=-15°C		mean	No Data	0.201818	0.211481	No Data	0.22125	0.22125
maximum 0 0.32 0.32 0 0.27 0.27 no of obs 0 22 0 0.17 0.17 0.17 no of obs 0 22 27 0 8 8 TC SFT79 <=-15°C		st dev	No Data	0.047972	0.047935	No Data	0.04051	0.04051
minimum 0 0.12 0.12 0 0.17 0.17 no of obs 0 22 27 0 8 8 TC SFT79 <=-15°C		maximum	0	0.32	0.32	0	0.27	0.27
no of obs 0 22 27 0 8 8 TC SFT'79 <=-15°C		minimum	0	0.12	0.12	0	0.17	0.17
TC SFT79 <=-15°C >-15°C All Temps <=-15°C >-15°C All Temps (All Configs) mean No Data 0.204815 0.205625 No Data 0.011738 0.011738 0.011738 minimum 0 0.33 0.33 0 0.26 0.26 minimum 0 0.09 0.09 0 0.23 0.23 no of obs 0 27 32 0 10 10 TC SFT79 <=-15°C		no of obs	0	22	27	0	8	8
TC SFT79 <=-15°C >-15°C All Temps <=-15°C >-15°C All Temps (All mean No Data 0.204815 0.205625 No Data 0.246 0.246 Configs) st dev No Data 0.057135 0.052667 No Data 0.011738 0.011738 maximum 0 0.33 0.33 0 0.223 0.23 moinimum 0 0.27 32 0 10 10 TC SFT79 <=-15°C								
mean No Data 0.204815 0.205625 No Data 0.246 0.246 Configs) st dev No Data 0.057135 0.052667 No Data 0.011738 0.011738 maximum 0 0.33 0.33 0 0.26 0.26 maximum 0 0.09 0.09 0 0.23 0.23 no f obs 0 27 32 0 10 10 TC SFT'79 <=-15°C	TC SFT'79		<=-15°C	> -15°C	All Temps	<=-15°C	> -15°C	All Temps
St dev No Data 0.057135 0.052667 No Data 0.011738 0.011738 0.011738 0.011738 0.011738 0.011738 0.011738 0.011738 0.011738 0.011738 0.011738 0.011738 0.026 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.246 0.243 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.24 0.016 0.24 0.24 <td>(All</td> <td>mean</td> <td>No Data</td> <td>0.204815</td> <td>0.205625</td> <td>No Data</td> <td>0.246</td> <td>0.246</td>	(All	mean	No Data	0.204815	0.205625	No Data	0.246	0.246
maximum 0 0.33 0.33 0 0.26 0.26 minimum 0 0.09 0.09 0 0.23 0.23 no of obs 0 27 32 0 10 10 TC SFT79 <=-15°C	Configs)	st dev	No Data	0.057135	0.052667	No Data	0.011738	0.011738
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		maximum	0	0.33	0.33	0	0.26	0.26
no of obs 0 27 32 0 10 10 TC SFT'79 <=-15°C		minimum	0	0.09	0.09	0	0.23	0.23
TC SFT79 <=-15°C >-15°C All Temps <==-15°C >-15°C All Temps (Config 3) mean No Data 0.221304 0.219286 No Data 0.246 0.246 st dev No Data 0.043621 0.040086 No Data 0.011738 0.011738 maximum 0 0.33 0.33 0 0.26 0.26 minimum 0 0.16 0.16 0 0.23 0.23 no of obs 0 23 28 0 10 10 IMAG <=-15°C		no of obs	0	27	32	0	10	10
$\begin{array}{c c c c c c c c c c c c c c c c c c c $								
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	TC SFT'79		<=-15°C	> -15°C	All Temps	<=-15°C	> -15°C	All Temps
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	(Config 3)	mean	No Data	0.221304	0.219286	No Data	0.246	0.246
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		st dev	No Data	0.043621	0.040086	No Data	0.011738	0.011738
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		maximum	0	0.33	0.33	0	0.26	0.26
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		minimum	0	0.16	0.16	0	0.23	0.23
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		no of obs	0	23	28	0	10	10
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			_					
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	IMAG	1	<=-15°C	> -15°C	All Temps	 <=-15°C	> -15°C	All Temps
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Force	mean	No Data	0.233684	0.241667	 No Data	0.243333	0.243333
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	(All	st dev	No Data	0.059462	0.05522	No Data	0.01633	0.01633
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Configs)	maximum	0	0.41	0.41	0	0.26	0.26
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		minimum	0	0.16	0.16	 0	0.22	0.22
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		no of obs	0	19	24	 0	6	6
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			4500	4500	A 11 T	 4500	4500	A.H. T
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	IMAG		<=-15°C	> -15°C	All Temps	 <=-15°C	> -15°C	All Temps
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Iorque	mean	No Data	0.154783	0.161429	No Data	0.178333	0.178333
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	(All Confirm)	st dev	No Data	0.045614	0.043861	 No Data	0.004082	0.004082
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Conligs)	maximum	0	0.33	0.33	 0	0.18	0.18
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		minimum na af aba	0	0.1	0.1	 0	0.17	0.17
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		ado io on	0	23	28	 0	0	0
IMAG Rean No Data 0.233684 0.241667 No Data 0.243333 0.2423 0.222 0.222 0.222 0.222 0.222 0.222 0.222 0.222 0.223 0.265 0.243333	IMAG		<- 15°C	> 15°C		 <- 15°C	> 15°C	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Force	moon	<=-15 C	0 233684	All Temps	 $\leq = 15 \text{ C}$	>-10 C	All Temps
$\begin{array}{c cccc} (COIIIIgs & St dev & NO Data & 0.039402 & 0.03322 & NO Data & 0.01033 & 0.01033 \\ \hline maximum & 0 & 0.41 & 0.41 & 0 & 0.26 & 0.26 \\ \hline minimum & 0 & 0.16 & 0.16 & 0 & 0.22 & 0.22 \\ \hline no of obs & 0 & 19 & 24 & 0 & 6 & 6 \\ \hline maximum & 0 & 0.16 & 0.16 & 0 & 0.22 & 0.22 \\ \hline no of obs & 0 & 19 & 24 & 0 & 6 & 6 \\ \hline maximum & 0 & 0.154783 & 0.161429 & No Data & 0.178333 & 0.178333 \\ \hline (Configs & st dev & No Data & 0.045614 & 0.043861 & No Data & 0.004082 & 0.004082 \\ \hline maximum & 0 & 0.33 & 0.33 & 0 & 0.18 & 0.18 \\ \hline minimum & 0 & 0.1 & 0.1 & 0 & 0.17 & 0.17 \\ \hline no of obs & 0 & 23 & 28 & 0 & 6 & 6 \\ \hline \end{array}$	Confige	et dov	No Data	0.233004	0.241007	 No Data	0.243333	0.243333
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	(Conings 3 & 7)	maximum		0.033402	0.03522		0.01000	0.01000
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	5 (1)	minimum	0	0.41	0.41	 0	0.20	0.20
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		no of obs	0	19	24	 0	6.22	6.22
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			0	10	27		0	0
Instruct Image Image <thimage< th=""> <</thimage<>	IMAG		<=-15℃	> -15°C	All Temps	 <=-15°C	> -15°C	All Temps
(Configs st dev No Data 0.045614 0.043861 No Data 0.004082 0.004082 3 & 7) maximum 0 0.33 0.33 0 0.18 0.18 minimum 0 0.1 0.1 0 0.17 0.17 no of obs 0 23 28 0 6 6	Torque	mean	No Data	0 154783	0 161429	No Data	0 178333	0 178333
3 & 7) maximum 0 0.33 0.33 0 0.18 0.18 ininimum 0 0.1 0.1 0 0.17 0.17 ininimum 0 23 28 0 6 6	(Configs	st dev	No Data	0.045614	0.043861	No Data	0.004082	0.004082
minimum 0 0.1 0.1 0 0.17 0.17 Ino of obs 0 23 28 0 6 6	3 & 7)	maximum	0	0.33	0.33	0	0.00	0.0018
		minimum	0	0.00	0.00	0	0.10	0.10
		no of obs	0	23	28	0	6	6

Table 3.7: Summary Results for Snow-Covered Packed Snow

3.5 Slush on Any Base Surface

Figure 3.20 provides summary results for slush on any base surface. Summary results are tabulated in Table 3.8. Detailed results are plotted in Appendix G.

Only a few data points are available, which limits the strength of the conclusions that can be drawn (Table 3.8). Furthermore, only very limited slush depth data are available. For the ERD results, slush depth data are available for only 10 of the 34 friction observations. The measured depths are highly variable, ranging from 8 mm to 50 mm. No slush depth data are available for correlation with the TC SFT'79 and IMAG friction data. This further limits the strength of the conclusions that can be drawn. Nevertheless, some preliminary observations can be made as follows:

- (1) Ranges of Variation The measured friction coefficients span a wide range for each device.
- (2) Friction Coefficient Magnitudes These tend to be higher than those for bare ice or bare packed snow.

3.6 Wet Pavement

Figure 3.21 provides summary results for wet pavement. Summary results are tabulated in Table 3.8. Detailed results are plotted in Appendix H. Only a few data points are available, which limits the strength of the conclusions that can be drawn (Table 3.8). Nevertheless, some preliminary observations can be made as follows:

- (1) Comparison to AIP The measured friction coefficients are generally higher than those in the AIP.
- (2) Ranges of Variation The measured friction coefficients span a wide range for each device.

3.7 Dry Pavement

Figure 3.22 provides summary results for dry pavement. Summary results are tabulated in Table 3.8. Detailed results are plotted in Appendix I. Although only a few data points are available (Table 3.8), some preliminary observations can be made as follows:

- (1) Comparison to AIP The measured friction factors are lower than those in the AIP.
- (2) Ranges of Variation The ranges for each device are similar to those in the AIP.
- (3) Wet vs. Dry Pavement The ERD indicated higher friction on average for wet pavement than for dry pavement (Table 3.8). This may reflect variations in texture among the different sites included in the observations used to establish the average.

Device	Slush or	n Any Base Surface	Wet	Pavement		Dry Pavement
ERD		All Temperatures	All Te	emperatures		All Temperatures
	mean	0.305882352		0.709130445		0.696923082
	st dev	0.121508638		0.079252929		0.065368777
	maximum	0.629999995		0.829999983		0.81000002
	minimum	0.090000004		0.540000021		0.589999974
	no of obs	34		23		13
TC SFT'79	-	All Temperatures				All Temperatures
(All	mean	0.229999997				0.875344826
Configs)	st dev	0.152970581				0.048130506
	maximum	0.569999993				1
	minimum	0.079999998				0.779999971
	no of obs	17				58
TC SFT'79	T	All Temperatures	All Te	emperatures		All Temperatures
(Config 3)	mean	0.236153843		0.807619049		0.905833331
	st dev	0.174381687	_	0.059405784		0.03752294
	maximum	0.569999993	_	0.920000017		1
	minimum	0.079999998	_	0.68000007		0.850000024
	no of obs	13		21		24
			_			A !! T
IMAG	1	All Temperatures				All Temperatures
Force	mean	0.27625	_			0.735652179
(All	st dev	0.149883289				0.063092598
Configs)	maximum	0.680000007	_			0.910000026
	minimum	0.109999999	_			0.589999974
	no of obs	16				46
	maan		_			
Torque	mean	0.210	_			0.09333333
(All Configo)	Stuev	0.127510577	_			0.050052157
Conings)	minimum	0.029999999	_			0.660000014
	no of obc	0.1099999999	-			0.009999974
		20				40
IMAG				amperatures		
Force	mean			0 600638205		0 735652170
(Configs	st dev	0.27023	_	0.030030233		0.753032179
(001111g3 3 & 7)	maximum	0.140000200	_	0.839999974		0.000002000
5 (1)	minimum	0.00000007		0.589999974		0.580000020
	no of obs	0.100000000	_	47		0.000000014
		10	-	···		
IMAG		All Temperatures		emperatures		All Temperatures
Torque	mean	0.218		0.624705884		0.69333333
(Configs	st dev	0.127510577		0.172108722		0.056052157
3 & 7)	maximum	0.6299999995		0.819999993		0.860000014
,	minimum	0.1099999999		0.050000001		0.589999974
	no of obs	20		51	-	48

Table 3.8: Summary Results for Slush, Wet Pavement and Dry Pavement

3.8 Direct Comparisons with the CRFI Values in the AIP

3.8.1 Presentation of Results

Figures 3.2 to 3.5 show summary results for the ERD, the TC SFT'79 in configuration 3, the IMAG Force in configurations 3 or 7, and the IMAG Torque in configurations 3 or 7, respectively. For reference, the CRFI values currently in the AIP are re-plotted in Figure 3.22.

3.8.2 Ice Surfaces

The following comments can be made:

(a) "Cold" (below -10°C) vs. "Warm" (at or above 0°C) Ice – The AIP values indicate a sharp distinction between cold and warm ice, with higher CRFIs for warm ice.

The devices do not show such a distinction. The ERD, the TC SFT'79 (configuration 3) and the IMAG Torque (configurations 3 or 7) all show higher CRFIs for warm ice than cold ice. The IMAG Force (configurations 3 or 7) indicates similar CRFIs for warm and cold ice.

(b) Sanded Ice – The AIP indicates that sanded ice can be expected to have a CRFI that is much larger than bare ice. Furthermore, it indicates that the CRFI for sanded ice will lie in a narrow range.

The devices gave CRFI values that spanned a wide range. The range of CRFIs measured for sanded ice was similar to that for bare ice.

3.8.3 Packed Snow

The following comments can be made:

(a) Effect of Temperature – The CRFIs in the AIP are much higher for "cold" packed snow (i.e., below -15°C).

The ERD and the IMAG both measured CRFIs that are not greatly different over the full range of temperatures. Data are not available for the TC SFT'79 at below -15°C, and thus, comparisons cannot be made for it.

(b) Packed Snow vs. Bare Ice – The CRFIs in the AIP are significantly higher for packed snow than for bare ice.

The measured values do not exhibit a clear difference between bare ice and bare packed snow, although they are slightly higher for packed snow.

(c) Snow on a Packed Snow Base – The AIP indicates that the CRFI for snowcovered packed snow will lie between the values for bare "warm" and "cold" packed snow.

The measured values for snow-covered packed snow are similar to those for bare packed snow.

3.8.4 Wet Pavement

The measured CRFIs are generally similar to those given in the AIP for damp pavement.



Figure 3.2: Summary Results for the ERD



Figure 3.3: Summary Results for the TC SFT'79 in Configuration 3



Figure 3.4: Summary Results for the IMAG Force in Configuration 3 or 7



Figure 3.5: Summary Results for the IMAG Torque in Configuration 3 or 7



RUNWAY SURFACE CONDITION (RSC) AND CRFI EQUIVILENT

Figure 3.6: CRFIs Given in the AIP for Various Surfaces [2] (repeated from Figure 2.2)



Figure 3.7: Friction Coefficients on Bare Ice: Summary Results



Figure 3.8: Friction Coefficients on Bare Ice Including Rough Ice: Summary Results



Figure 3.9: Friction Coefficients on Bare Packed Snow: Summary Results



Figure 3.10: Friction Coefficients on Sanded Ice: Summary Results



Figure 3.11: Friction Coefficients on Sanded Ice Including Rough Ice: Summary Results



Figure 3.12: Friction Coefficients on Snow Covered Ice (All Depths of Snow Cover): Summary Results







Figure 3.14: Friction Coefficients on Snow Covered Ice Including Rough Ice (All Depths of Snow Cover): Summary Results



Figure 3.15: Friction Coefficients on Snow Covered Ice Including Rough Ice (Snow Cover 10 mm or Less Thick): Summary Results



Figure 3.16: Friction Coefficients on Snow Covered Pavement (All Depths of Snow Cover): Summary Results

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Figure 3.18: Friction Coefficients on Snow Covered Packed Snow (All Depths of Snow Cover): Summary Results



Figure 3.19: Friction Coefficients on Snow Covered Packed Snow (Snow Cover 10 mm or Less Thick): Summary Results



Figure 3.20: Friction Coefficients for Slush on any Base Surface: Summary Results



Figure 3.21: Friction Coefficients on Wet Pavement: Summary Results



Figure 3.22: Friction Coefficients on Dry Pavement: Summary Results

4. CORRELATION AMONG DEVICES BY SURFACE TYPE

4.1 Results: ERD vs. TC SFT'79

Figures 4.1, 4.2, and 4.3 show results for all surfaces, bare surfaces only, and contaminated surfaces only, respectively. More detailed plots are contained in Appendix J, showing a breakdown by surface type and base type. General comparisons are shown in Table 4.1.

It is evident that the largest scatter occurs for the contaminated surfaces. Compare Figures 4.2 and 4.3. This probably reflects forces due to contaminant drag that are likely to be more significant for the ERD (as it is a locked-wheel test).

	Tuble hit Summary comparison Lite (5) 10 511 ()									
Surface Type	Friction Level	Comparison								
Bare	All friction	TC SFT'79 readings about 10% higher than the ERD								
	levels	ones								
Contaminated	Less than about 0.4	 Relationship is highly scattered Generally, the ERD read higher than did the TC SFT'79 								
Contaminated	Greater than about 0.4	 Relationship is highly scattered Generally, the ERD read lower than did the TC SFT'79 								

 Table 4.1: Summary Comparison: ERD vs. TC SFT'79



Figure 4.1: Correlation of ERD to TC SFT'79: All Surfaces



Figure 4.2: Correlation of ERD to TC SFT'79: Bare Surfaces



Figure 4.3: Correlation of ERD to TC SFT'79: Contaminated Surfaces

4.2 Results: ERD vs. IMAG Force

Figures 4.4, 4.5, and 4.6 show results for all surfaces, bare surfaces only, and contaminated surfaces only, respectively. More detailed plots are contained in Appendix K, showing a breakdown by surface type and base type. General comparisons are shown in Table 4.2.

As was the case for the TC SFT'79, the largest scatter occurs for the contaminated surfaces. Compare Figures 4.5 and 4.6. This probably reflects forces due to contaminant drag that are likely to be more significant for the ERD (as it is a locked-wheel test).

Surface Type	Friction Level	Comparison								
Bare	All friction	IMAG Force readings about 10% higher than the ERD								
	levels	ones								
Contaminated	Less than about	• Relationship is highly scattered								
	0.4	• Generally, the ERD read higher than did the IMAG								
		Force								
Contaminated	Greater than	• Relationship is highly scattered								
	about 0.4	• Generally, the ERD read lower than did the IMAG								
		Force								

Table 4.2:	Summary	Com	parison:	ERD	vs.	IMA	G]	Force
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Figure 4.4: Correlation of ERD to IMAG Force: All Surfaces



Figure 4.5: Correlation of ERD to IMAG Force: Bare Surfaces



Figure 4.6: Correlation of ERD to IMAG Force: Contaminated Surfaces
4.3 Results: ERD vs. IMAG Torque

Figures 4.7, 4.8, and 4.9 show results for all surfaces, bare surfaces only, and contaminated surfaces only, respectively. More detailed plots are contained in Appendix L, showing a breakdown by surface type and base type. General comparisons are shown in Table 4.3.

As was the case for the other comparisons made to date, the largest scatter occurs for the contaminated surfaces. Compare Figures 4.8 and 4.9. This probably reflects forces due to contaminant drag that are likely to be more significant for the ERD (as it is a locked-wheel test).

Table 4.5. Summary Comparison. EKD vs. INFAO TOTQUE						
Surface Type	Friction Level	Comparison				
Bare	All friction	IMAG Torque readings slightly higher (less than				
	levels	10%) than the ERD ones				
Contaminated	Less than about	• Relationship is highly scattered				
	0.4	• Generally, the ERD read higher than did the				
		IMAG Torque				
Contaminated	Greater than	• Relationship is highly scattered				
	about 0.4	• Generally, the ERD read lower than did the				
		IMAG Torque				

 Table 4.3:
 Summary Comparison: ERD vs. IMAG Torque



Figure 4.7: Correlation of ERD to IMAG Torque: All Surfaces



Figure 4.8: Correlation of ERD to IMAG Torque: Bare Surfaces



Figure 4.9: Correlation of ERD to IMAG Torque: Contaminated Surfaces

4.4 Results: TC SFT'79 vs. IMAG Force

Figures 4.10, 4.11, and 4.12 show results for all surfaces, bare surfaces only, and contaminated surfaces only, respectively. More detailed plots are contained in Appendix M, showing a breakdown by surface type and base type. General comparisons are shown in Table 4.4.

The scatter is considerably less for this comparison than for all of the ones made with the ERD. Furthermore, the scatter is not significantly different between the contaminated and the bare surfaces. Compare Figures 4.11 and 4.12. This probably reflects the fact that both of these devices utilize a rolling, braked wheel to measure friction, and thus they are better able to "process" contaminants than is the ERD.

Surface Type	Friction Level	Comparison		
Bare	Less than about 0.4	IMAG Force readings generally lower than the TC		
		SFT'79 ones		
Bare	Greater than about	IMAG Force readings generally higher than the TC		
	0.4	SFT'79 ones		
Contaminated	Less than about 0.4	Generally, the TC SFT'79 read higher than did the		
		IMAG Force		
Contaminated	Greater than about	Generally, the TC SFT'79 read lower than did the		
	0.4	IMAG Force		

Table 4.4: Summary Comparison: TC SFT'79 vs. IMAG Force



Figure 4.10: Correlation of TC SFT'79 to IMAG Force: All Surfaces



Figure 4.11: Correlation of TC SFT'79 to IMAG Force: Bare Surfaces



Figure 4.12: Correlation of TC SFT'79 to IMAG Force: Contaminated Surfaces

4.5 Results: TC SFT'79 vs. IMAG Torque

Figures 4.13, 4.14, and 4.15 show results for all surfaces, bare surfaces only, and contaminated surfaces only, respectively. More detailed plots are contained in Appendix N, showing a breakdown by surface and base type. General comparisons are shown in Table 4.5.

As was the case for the IMAG force (section 4.4), the scatter is considerably less for this comparison than for all those made with the ERD. Furthermore, the scatter is not significantly different between the contaminated and the bare surfaces. Compare Figures 4.14 and 4.15. This probably reflects the fact that both of these devices utilize a rolling, braked wheel to measure friction, and thus they are better able to "process" contaminants than is the ERD.

Surface Type	Friction Level	Comparison		
Bare	All friction	IMAG Torque readings generally higher than the TC		
	levels	SFT'79 ones		
Contaminated	All friction	IMAG Torque readings generally higher than the TC		
	levels	SFT'79 ones		

 Table 4.5: Summary Comparison: TC SFT'79 vs. IMAG Torque



Figure 4.13: Correlation of TC SFT'79 to IMAG Torque: All Surfaces



Figure 4.14: Correlation of TC SFT'79 to IMAG Torque: Bare Surfaces



Figure 4.15: Correlation of TC SFT'79 to IMAG Torque: Contaminated Surfaces

4.6 Results: IMAG Force vs. IMAG Torque

Figures 4.16, 4.17, and 4.18 show results for all surfaces, bare surfaces only, and contaminated surfaces only, respectively. More detailed plots are contained in Appendix O, showing a breakdown by surface type and base type. General comparisons are shown in Table 4.6. This comparison showed the least scatter, probably because:

- (a) IMAG Force and IMAG Torque are both part of the same device.
- (b) IMAG utilizes a rolling, braked wheel to measure friction, which allows it to "process" contaminants. This is probably the reason the scatter is not significantly different between the contaminated and the bare surfaces. Compare Figures 4.17 and 4.18.

Surface Type	Friction Level	Comparison		
Bare	All friction	IMAG Torque readings always lower than the		
	levels	IMAG Force ones		
Contaminated	All friction	IMAG Torque readings always lower than the		
	levels	IMAG Force ones		

fable 4.6: Summa	y Compa	rison: IMA	G Force vs	. IMAG Torque
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It is also evident that:

- (a) IMAG Force and IMAG Torque are highly correlated to each other.
- (b) The IMAG Force reading is always higher than the IMAG Torque one. This is to be expected as the IMAG Force reading is determined by adding the contaminant drag to the horizontal braking forces applied to the measuring wheel. It is noteworthy that the relationship between the IMAG Torque and IMAG Force is generally similar for both the bare and the contaminated surfaces. (Figures 4.17 and 4.18). This suggests that the contaminant drag is an important part of the total horizontal forces applied to the measuring wheel even for the bare surfaces.



Figure 4.16: Correlation of IMAG Force to IMAG Torque: All Surfaces



Figure 4.17: Correlation of IMAG Force to IMAG Torque: Bare Surfaces



Figure 4.18: Correlation of IMAG Force to IMAG Torque: Contaminated Surfaces

5. CONCLUSIONS AND RECOMMENDATIONS

5.1 Conclusions

The results obtained from the JWRFMP were used to investigate the effect of surface conditions on the friction coefficient measured by the ERD, the TC SFT'79, and the IMAG. Two types of analyses were conducted as follows:

- (a) Analyses for individual surfaces Where possible, the friction coefficients obtained from the devices were compared to the guideline CRFIs given in the AIP.
- (b) Correlations among the devices.
- 5.1.1 Analyses for Individual Surfaces

The results varied from device to device and from surface to surface, which makes it difficult to infer general conclusions.

It was commonly observed that the ranges of values observed in the JWRFMP were larger than those given in the AIP.

5.1.2 Correlations among the Devices

The results varied from device to device and from surface to surface, which makes it difficult to infer general conclusions.

It was noted that:

- (a) ERD readings on contaminated surfaces were generally higher and more scattered on contaminated surfaces than those for the TC SFT'79 and the IMAG. This probably reflects the fact that the ERD is locked-wheel test.
- (b) TC SFT'79 and the IMAG showed good correlation for all surfaces.

5.2 Recommendations

This was an exploratory project that was aimed at investigating general trends and relationships. The results obtained here should be followed up with more detailed quantitative analyses to investigate issues such as:

- (a) Variability among the results for different surfaces.
- (b) Degree of confidence that one could have in friction coefficients inferred solely from surface descriptions, in comparison to data obtained with friction-measuring devices.

REFERENCES

- [1] Comfort, G., and Trott, B., 2002, *Joint Winter Runway Friction Test Program Database Manual*, prepared by Fleet Technology Limited for the Transportation Development Centre on behalf of Aerodrome Safety Branch of Civil Aviation, Transport Canada.
- [2] AIP, 2002, Aeronautical Information Publication, Air 1-15, Table 4, TP 2300.
- [3] Comfort, G., and Gong, Y., 1998, *Analysis of the Friction Factors Measured by the Ground Vehicles at the 1998 North Bay Trials*, TP 13366E Transportation Development Centre, Transport Canada.

APPENDIX A

RESULTS FOR BARE ICE

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Appendix A.1: Histograms Appendix A.2: Trend Plots vs. Surface Temperature

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A.1-4: ERD TC SFT'79 (All Configurations) Readings on Bare and Rough Ice: Effect of Temperature



A.1-5: TC SFT'79 (Configuration 3) Readings on Bare Ice: Effect of Temperature



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APPENDIX A.2

TREND PLOTS VS. SURFACE TEMPERATURE



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